

Using the 'ripple technique' to evaluate residual errors in waveguide VNAs

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Overview

This presentation aims to provide answers to **two questions**:

Q1: Does the ripple technique, as described in the EURAMET VNA Guide cg-12, work when applied to waveguide?

Q2: If "yes", why not include it as part of the revision of this Guide?



Outline

- What is the ripple technique?
- How can we test it in waveguide?
- Experiment description
- Results
- Summary



- A practical method for evaluating residual systematic errors remaining in a Vector Network Analyser after calibration (i.e. after the error-correction process has been applied by the VNA/user)
- The residual errors are due to the error correction process being less than perfect
- The ripple technique provides an evaluation of the residual Directivity and Test Port Match error terms for each of the VNA's calibrated test ports
- These can be major contributing error terms to the VNA's overall measurement uncertainty





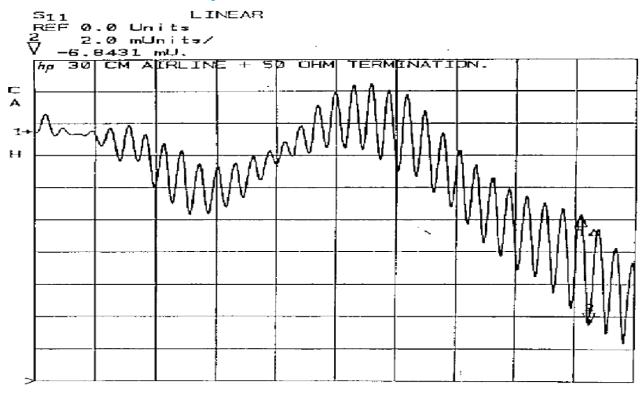
- The existing EURAMET VNA Guide cg-12 recommends using the ripple technique in coax
 - 7 mm (including Type-N) and 3.5 mm
- It also says:
 - "The procedure may have to be modified for other connector types, including waveguide transmission line."



- According to the EURAMET Guide, in 7 mm and 3.5 mm coax:
 - Residual Directivity assessed using:
 - Section of precision line + 'matched' load
 - Residual Test Port Match assessed using:
 - Section of precision line + short-circuit



Residual Directivity



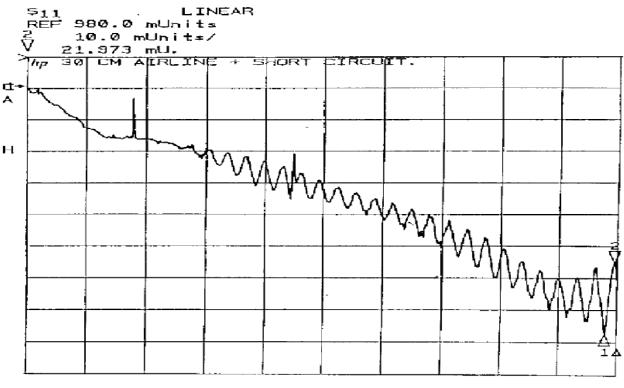
Start frequency: 2.000 GHz

Stop frequency: 18.000 GHz

Figure 1: A non-perfect 50 Ω load is connected to a 30 cm airline. The other side of the airline is attached to port 1. This figure shows which kind of typical response will be obtained measuring S11 as function of frequency. From the ripple an effective directivity can be determined.



Residual Test Port Match



Start frequency: 2.000 GHz

Stop frequency: 18.000 GHz

Figure 2: A short is connected to a 30 cm airline. The other side of the airline is attached to port 1. This figure shows which kind of typical response will be obtained measuring S11 as function of frequency. From the ripple an effective source match can be determined.



How can we test it in waveguide?

- Residual **Directivity** assessed using:
 - Section of precision waveguide + 'matched' load
- Residual Test Port Match assessed using:
 - Section of precision waveguide + short-circuit







Experiment description

- Pick a waveguide band (X-band: 8.2 GHz to 12.4 GHz)
- Do three types of VNA calibration:
 - TRL (Thru-Reflect-Line)
 - TRL (using a poor quality line)
 - TRM (Thru-Reflect-Match)
- Use the section of precision waveguide with matched load(s) and short to determine residual directivity and test port match, respectively

(choice of 2 matched loads: L1 and L2)

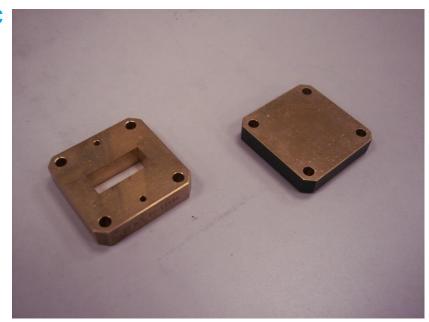






Experiment description – CAL 1: 'good' TRL cal

- The TRL calibration uses the Line standard to define the characteristic impedance of the calibrated VNA
- This leads to good quality calibrations (i.e. small residual errors)
- A good reference calibration, defining state-of-the-art





Experiment description - CAL 2: 'poor' TRL cal

- A poor quality line is used as the Line standard
- This will lead to increased residual errors because the calibration standards are less well defined
- Expect residual directivity and test port match to be larger than the 'good' TRL

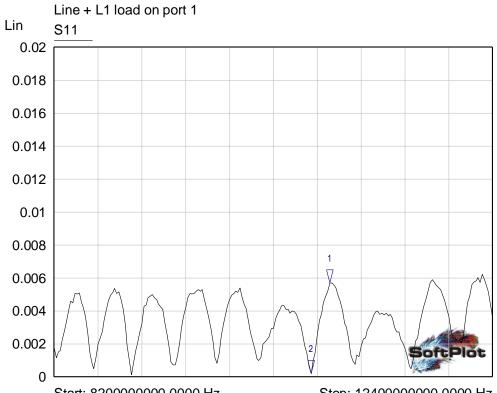


Experiment description – CAL 3: TRM cal

- A 'matched load' is used to set the impedance on the system
- A different calibration 'matched load' has been used for each test port (L1 and L2)
- Residual errors may be different due to these difference calibration loads



Results – CAL 1: Good TRL cal – Port 1 directivity (using L1)



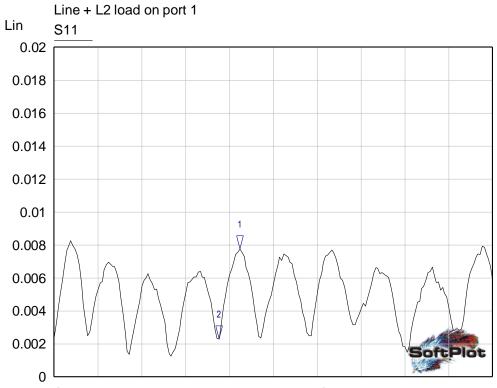
Start: 8200000000.0000 Hz 17/10/2014 09:43:43 Stop: 12400000000.0000 Hz HP8510C

Mkr	Trace	X-Axis	Value	Notes
1 🎖	S11	10840000000.0000 Hz	5.69 mLin	
2 🏹	S11	10660000000.0000 Hz	197.46 uLin	

Directivity ≈ 0.003



Results – CAL 1: Good TRL cal – Port 1 directivity (using L2)



Directivity ≈ 0.003

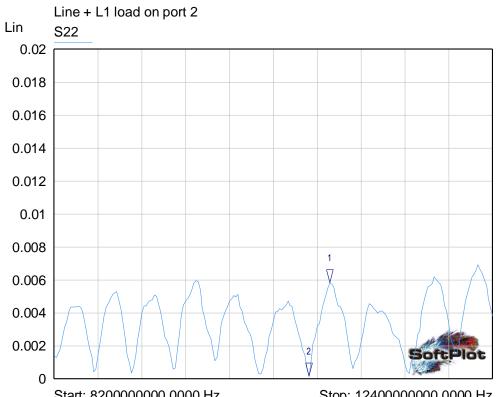
Start: 8200000000.0000 Hz 17/10/2014 11:21:55

Stop: 12400000000.0000 Hz HP8510C

Mkr	Trace	X-Axis	Value	Notes
1 🎖	S11	9980000000.0000 Hz	7.78 mLin	
2 🏹	S11	9780000000.0000 Hz	2.31 mLin	



Results – CAL 1: Good TRL cal – Port 2 directivity (using L1)



Directivity ≈ 0.003

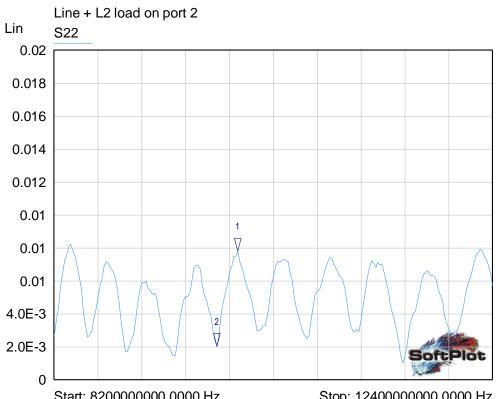
Start: 8200000000.0000 Hz 17/10/2014 11:31:24 Stop: 12400000000.0000 Hz HP8510C

Mkr	Trace	X-Axis	Value	Notes
1 🎖	S22	10840000000.0000 Hz	5.84 mLin	
2 🎖	S22	10640000000.0000 Hz	171.34 uLin	





Results – CAL 1: Good TRL cal – Port 2 directivity (using L2)



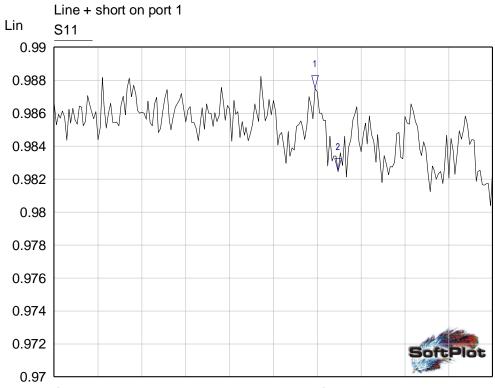
Directivity ≈ 0.003

Start: 8200000000.0000 Hz 17/10/2014 11:34:24 Stop: 12400000000.0000 Hz HP8510C

Mkr	Trace	X-Axis	Value	Notes
1 🎖	S22	9960000000.0000 Hz	7.80 mLin	
2 🎖	S22	9760000000.0000 Hz	2.04 mLin	



Results - CAL 1: Good TRL cal - Port 1 Test Port Match



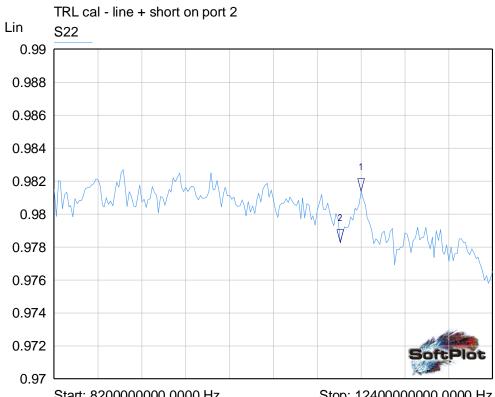
Start: 8200000000.0000 Hz 17/10/2014 11:25:50 Stop: 12400000000.0000 Hz HP8510C

Mkr	Trace	X-Axis	Value	Notes
1 🎖	S11	10700000000.0000 Hz	987.50 mLin	
2 🏹	S11	10920000000.0000 Hz	982.45 mLin	

National Measurement System Test Port Match ≈ 0.003



Results – CAL 1: Good TRL cal – Port 2 Test Port Match



Start: 8200000000.0000 Hz 17/10/2014 12:15:34

Stop: 12400000000.0000 Hz HP8510C

Mkr	Trace	X-Axis	Value	Notes
1 🎖	S22	11140000000.0000 Hz	981.38 mLin	
2 🎖	S22	10940000000.0000 Hz	978.26 mLin	

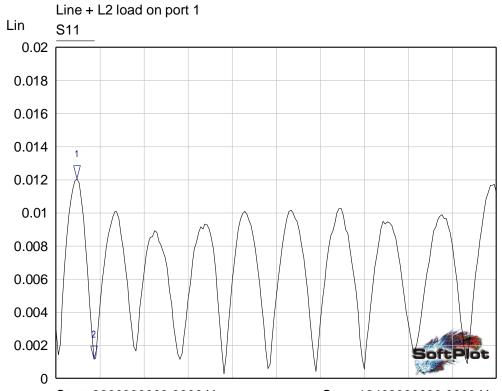
National Measurement **System**

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Test Port Match ≈ 0.002



Results – CAL 2: Poor TRL cal – Port 1 directivity (using L2)



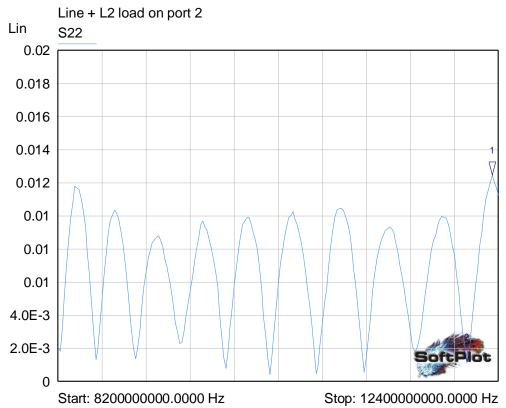
Directivity ≈ 0.006

Start: 8200000000.0000 Hz 17/10/2014 13:27:12 Stop: 12400000000.0000 Hz HP8510C

Mkr	Trace	X-Axis	Value	Notes
1 🎖	S11	840000000.0000 H	z12.07 mLin	
2 🎖	S11	8560000000.0000 H	z1.17 mLin	



Results – CAL 2: Poor TRL cal – Port 2 directivity (using L2)



Directivity ≈ 0.006

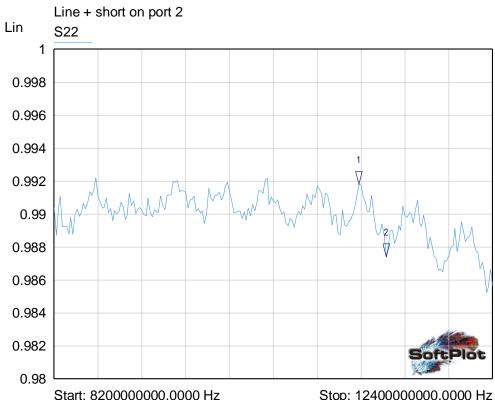
17/10/2014 13:39:36

HP8510C

Mk	r Trace	X-Axis	Value	Notes
1 🗸	S22	12340000000.0000 H	z12.47 mLin	
2 \	S22	12100000000.0000 H	z1.17 mLin	



Results - CAL 2: Poor TRL cal - Port 2 Test Port Match



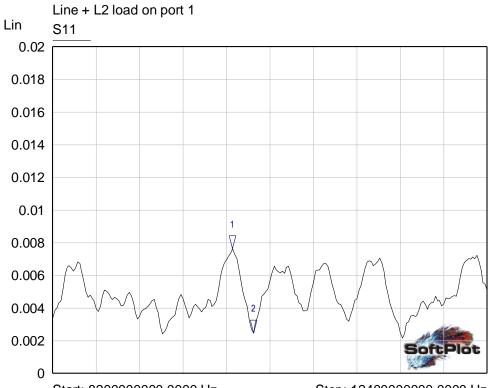
Test Port Match ≈ 0.002

Start: 8200000000.0000 Hz 17/10/2014 13:34:03 Stop: 12400000000.0000 Hz HP8510C

Mk	r Trace	X-Axis	Value	Notes
1 🗸	S22	11120000000.0000 Hz	991.80 mLin	
2 \	S22	11380000000.0000 Hz	987.42 mLin	



Results – CAL 3: TRM cal – Port 1 directivity (using L2)



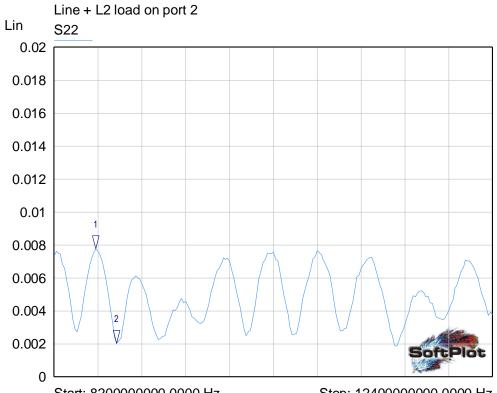
Start: 8200000000.0000 Hz 17/10/2014 12:07:09 Stop: 12400000000.0000 Hz HP8510C

Mkr	Trace	X-Axis	Value	Notes
1 🎖	S11	9940000000.0000 Hz	z 7.65 mLin	
2 🏹	S11	10140000000.0000 H	H2.46 mLin	

Directivity ≈ 0.003



Results – CAL 3: TRM cal – Port 2 directivity (using L2)



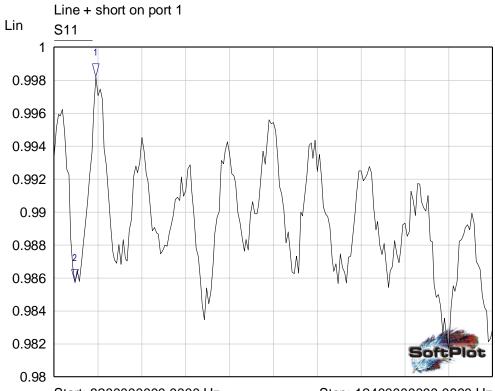
Start: 8200000000.0000 Hz 17/10/2014 12:21:57 Stop: 12400000000.0000 Hz HP8510C

I	Mkr	Trace	X-Axis	Value	Notes
	1 🏻	S22	8600000000.0000 Hz	7.78 mLin	
2	2 🗸	S22	8800000000.0000 Hz	2.02 mLin	

Directivity ≈ 0.003



Results – CAL 3: TRM cal – Port 1 Test Port Match



Start: 8200000000.0000 Hz 17/10/2014 12:09:50 Stop: 12400000000.0000 Hz HP8510C

Mkr	Trace	X-Axis	Value	Notes
1 🎖	S11	8600000000.0000 Hz	998.22 mLin	
2 🏹	S11	8400000000.0000 Hz	985.74 mLin	

Test Port Match ≈ 0.006



Results – Summary values

Calibration type	Residual Directivity	Residual Test Port Match
Good TRL	0.003	0.003
Poor TRL	0.006	0.003
TRM	0.003	0.006



Summary

Q1: Does the ripple technique, as described in the EURAMET VNA Guide cg-12, work when applied to waveguide?







Summary

Q2: Why not include it as part of the revision of this Guide?

- There is no good reason why not to include it
- There are good reasons to include it:
 - It will help laboratories to evaluate uncertainties in waveguide measurements
 - It will help laboratories to obtain ISO 17025 accreditation for waveguide measurements

These are both very good scientific and commercial reasons for including waveguide in the upcoming revision of the Guide





Acknowledgement



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